

## SPECIFICATION

### Title of the Invention

MAGNETIC RECORDING MEDIUM, THE MANUFACTURING  
5 METHOD AND MAGNETIC RECORDING APPARATUS USING THE SAME

### Background of the Invention

This invention relates to a magnetic recording  
medium which has excellent reliability and in which  
10 magnetic recording is performed with high density, a  
manufacturing method thereof and a magnetic disc device  
used in an auxiliary storage apparatus of a computer.

A magnetic disc apparatus used in a storage  
apparatus of a large-scale computer, a work station, a  
15 personal computer and the like has been yearly  
increased in its importance and developed into a mass-  
stored and small sized device. Increasing of recording  
density is essential to the development of the magnetic  
disc apparatus into mass-stored and small-sized  
20 apparatus. As the technology for realizing the  
development into the mass-stored and small-sized device,  
cited is reduction in distance between a magnetic  
recording layer of a magnetic recording medium and a  
magnetic head.

25 The magnetic recording medium manufactured by  
sputtering has been provided with a protective coating  
heretofore for the purpose of protecting a magnetic  
film from sliding of a magnetic head. Thinning of the

protective coating and reduction of distance between the surface of the protective coating and the magnetic head are the most effective means for more decreasing the distance between a magnetic recording layer and the magnetic head. For this protective coating, carbon manufactured by DC sputtering, RF sputtering (Japanese Patent Laid Open Hei 5-174369), or CVD (Japanese Patent Laid-Open No. Hei 4-90125) is most generally used, and a method of mixing nitrogen atoms, hydrogen atoms and the like in the film to obtain a protective coating more excellent in strength (Japanese Patent Laid-Open No. Sho 62-246129) has been generally adopted. Further, it is general to use perfluoropolyether liquid lubricant for the purpose of reducing friction between the magnetic head and the magnetic recording medium.

As a general method for thinning, cited is to apply diamond-like carbon (DLC) using ion beam deposition (IBD) or chemical vapor deposition (CVD) for a protective coating. DLC, however, bonding strength of carbon atoms and hydrogen atoms in the thin film is generally strong and also its network has higher continuity as compared with the carbon protective coating provided by the sputtering. Therefore, the problem is that the bonding strength to perfluoropolyether lubricant applied to the protective coating is weak owing to fewer functional groups.

One of performance indexes of the magnetic recording device using the magnetic recording medium is

the data transfer rate. The data transfer rate largely depends on the data access time. The access time is composed of the seek time and the rotation waiting time, and to shorten the rotation waiting time by increasing the rotating speed of a magnetic recording medium leads to the improvement in the data transfer rate.

When the rotating speed of the magnetic recording medium is increased, however, centrifugal force is applied to the liquid lubricant on the DLC protective coating of the magnetic recording medium so that as the result of the problem that the bonding strength is weak, the liquid lubricant is driven away toward the outer peripheral part of the magnetic recording medium until it is shaken off from the magnetic recording medium (hereinafter referred to as spin-off). Consequently, the problem encountered is that the lubricant on the magnetic recording medium is decreased to increase the frictional force between the magnetic recording medium and the magnetic head and cause a crash.

In order to solve the problems, attempts have been made to apply surface treatment to the protective coating so as to increase the bonding strength. Japanese Patent Laid-Open No. Sho 62-150526 and Japanese Patent Laid-Open No. Sho 63-2117 disclose that the surface is subjected to plasma treatment. Japanese Patent Laid-Open No. Hei 4-6624 discloses that the surface is subjected to ultraviolet treatment, water treatment, ozonization or the like. Further, Japanese

Patent Laid-Open No. Sho 63-2117, Japanese Patent Laid-Open No. Hei 9-30596, Japanese Patent Laid-Open No. Hei 8-225791, Japanese Patent Laid-Open No. Hei 7-210850 and Japanese Patent Laid-Open No. Hei 5-174354 are  
5 similar to the above, and all of these disclose that after the protective layer is formed, the surface thereof is subjected to some treatment. These methods, however, have the problem that it is difficult to uniformly treat the whole surface, one additional  
10 process is needed in the work, and besides the adhesion of the lubricant is insufficient.

#### Summary of the Invention

The present invention has been made in view of  
15 the above circumstances and provides a magnetic recording medium which is increased in the chemical bonding strength of a protective coating layer and liquid lubricant not to cause a decrease in liquid lubricant due to spin-off under high speed rotation.

20 Further, the invention provides a manufacturing method for the above magnetic recording medium.

Further, the invention provides a magnetic storage apparatus suitable for reconciling high speed rotation and high reliability by using the above  
25 magnetic recording medium.

To solve the above problems, the invention mainly adopts the following constitution.

According to the invention, a magnetic recording

medium is characterized in that the magnetic recording medium has a magnetic film formed on a non-magnetic substrate by intercalating at least an under layer , and the proportion of functional groups per 100 carbon atoms in the diamond-like carbon protective coating mainly composed of carbon, which protects the magnetic film, exceeds 20%.

In the case where a lubricating film of perfluoropolyether having at least one functional group is provided on the protective coating, bonding performance between the protective coating and the lubricating film is excellent.

According to the invention, a manufacturing method for the magnetic recording medium is characterized in that in the manufacturing method for the magnetic recording medium having a magnetic film formed on a non-magnetic substrate by intercalating at least an under layer , when a protective coating mainly composed of carbon for protecting the magnetic film is formed by an ion beam method or a chemical vapor deposition method, at least one gas among  $\text{CO}_2$ ,  $\text{NO}_2$ ,  $\text{N}_2\text{O}$  is added.

In the case where the protective coating is diamond-like carbon, the bonding performance between the protective coating and the lubricating film is especially improved.

In the case of forming the protective coating by the ion beam method or the chemical vapor deposition

method, it is preferable to use at least one of N<sub>2</sub>, Ne, Ar, Kr and Xe and hydrocarbon gas or hydrocarbon gas.

In the manufacturing method for the magnetic recording medium having a magnetic film formed on a non-magnetic substrate by intercalating at least an under layer , at the time of forming a diamond-like carbon protective coating mainly composed of carbon for protecting the magnetic film by an ion beam method or a chemical vapor deposition method, one gas among CO<sub>2</sub>, NO<sub>2</sub>, N<sub>2</sub>O may be added.

According to the invention, a magnetic storage device is characterized that the device includes the magnetic recording medium, a driving part for driving the magnetic recording medium, a magnetic head having a recording part and a reproducing part, a recording reproducing signal processing part for giving and receiving a signal to and from the magnetic head, and a magnetoresistive head as a reproducing part of the magnetic head.

#### Brief Description of the Drawings

Preferred embodiments of the present invention will be described in detail based on the followings, wherein

Fig. 1 is a typical sectional view of a magnetic recording medium according to the embodiment of the invention;

Fig. 2 is a schematic diagram of a protective

coating forming chamber 21;

Fig. 3 is a diagram showing the comparison of performance between the magnetic recording media provided according to the embodiment and the comparative example of the invention;

Fig. 4 is a diagram showing the general construction of a magnetic storage device;

Fig. 5 is a typical perspective view of a magnetic head;

Fig. 6 is a diagram showing the sectional structure of a magnetoresistive sensor; and

Fig. 7 is a sectional view of a sensor using a spin valve head.

#### Description of the Preferred Embodiments

First, the function, constitution and operation of the invention will be described in brief in the following. In the manufacturing method for the magnetic recording medium having a magnetic film, a protective coating mainly composed of carbon for protecting the magnetic film and a lubricating film of perfluoropolyether having at least one functional group provided on a substrate, at the time of forming the protective coating by an ion beam method using at least one of  $N_2$ , Ne, Ar, Kr, Xe and hydrocarbon gas, or only the hydrocarbon gas or a CVD method, the bonding performance between the protective coating and the lubricating film is improved by adding at least one gas

among CO<sub>2</sub>, NO<sub>2</sub>, N<sub>2</sub>O.

In the magnetic recording medium provided by the above method, the proportion of functional groups per 100 carbon atoms in the protective coating can be over 20%.

The magnetic storage apparatus of the invention includes the magnetic recording medium, a driving part for driving the magnetic recording medium, a magnetic head formed by a recording part and a reproducing part, a unit for moving the magnetic head relatively to the magnetic recording medium, a signal input unit for inputting a signal to the magnetic head and a recording reproducing signal processing unit for reproducing an output signal from the magnetic head, wherein the reproducing part of the magnetic head is formed by a magnetoresistive head, and the magnetic recording medium is formed by the magnetic recording medium including the protective coating having the above characteristic quality, hardness and thickness.

Further, the magnetoresistive sensor part of the magnetoresistive head is formed between two shield layers which are spaced from each other at a distance of 0.2  $\mu$ m or less and made of soft magnetic substance, and the product  $B_r \times t$  of the thickness (t) of the magnetic layer of the thus constructed magnetic recording medium and the residual flux density  $B_r$  measured by applying a magnetic field in the relative traveling direction of the magnetic head to the



magnetic recording medium in recording ranges from 3.2mA (40 gauss micron) to 9.6mA (120 gauss micron) both inclusive.

5 The reason why the magnetoresistive sensor part of the magnetoresistive head is to be formed between two shield layers which are spaced from each other at a distance of  $0.2\mu\text{m}$  or less and made of soft magnetic substance is that in the magnetic storage apparatus having the maximum track recording density of 220kFCI, 10 sufficient reproducing output cannot be obtained. The distance between two shield layers made of soft magnetic substance is preferably  $0.12\mu\text{m}$  or more in view of working easiness.

15 The reason why the product  $B_r \times t$  of the thickness ( $t$ ) of the magnetic layer of the thus constructed magnetic recording medium and the residual flux density  $B_r$  measured by applying a magnetic field in the relative traveling direction of the magnetic head to the magnetic recording medium in recording 20 ranges from 3.2mA (40 gauss micron) to 9.6mA (120 gauss micron) both inclusive is that when the  $B_r \times t$  is 3.2mA (40 gauss micron), the risk of reproducing wrong information becomes higher due to lowering of reproducing output caused by being left for long time 25 after recording, and when it exceeds 9.6mA (120 gauss micron), it becomes difficult to overwrite in recording.

Further, by forming at least two layers of under layers in the magnetic recording medium, the crystal

orientation of the magnetic layer may be controlled.  
By forming such multiple under layer, the influence of  
atomic diffusion from the under layer to the magnetic  
layer can be remarkably reduced, and simultaneously the  
5 crystallinity of the under layer close to the magnetic  
layer can be improved, and the adhesion between the  
magnetic layer and the under layer becomes strong so as  
to obtain high sliding resisting performance. Further,  
since the surface of the under layer close to the  
10 magnetic layer has no atomic periodic array extending  
over a long distance, the crystal grains of the  
magnetic layer formed thereon may be refined and also  
the crystal orientation may be controlled. Thus, the  
mean particle diameter of crystal constituting the  
15 magnetic layer is controlled to 15nm or less suitable  
for reduction of noise, very fine size, and  
simultaneously the direction of the axis of easy  
magnetization may be controlled to be parallel to the  
film surface suitable for in-plane magnetic recording.

20 The magnetoresistive head used in the magnetic  
storage apparatus of the invention is formed by a  
magnetoresistive sensor including plural conductive  
magnetic layers causing a large resistance change due  
to a relative change of mutual magnetizing directions  
25 by an external magnetic field, and a conductive non-  
magnetic layer disposed between the conductive magnetic  
layers. The reason why the thus constructed  
reproducing head is used is that a signal recorded at

the maximum track recording density exceeding 300kFCI is stably reproduced to obtain signal output.

Further, the magnetoresistive head is formed on a magnetic head slider, in which the area of the floating surface rail is equal to or smaller than  $1.00\text{mm}^2$  and the mass is equal to or less than 2mg to achieve the invention. The reason why the area of the floating surface rail is equal to or smaller than  $1.00\text{mm}^2$  is that the probability of colliding with the projection is reduced, and simultaneously, the shock resistance reliability can be improved by setting the mass equal to or less than 2mg. Thus, the recording density of 50 giga-bit per  $1\text{in}^2$  and high shock resistance may be consistent with each other.

The embodiments of the invention will now be described in detail. Fig. 1 shows one embodiment of the invention.

<Embodiment 1>

First, a soda lime glass substrate 1 (outside diameter of 84mm, inside diameter of 25mm and thickness of 1.1mm) to be used is sufficiently washed. This substrate is introduced into a vacuum vessel evacuated to about  $5.3 \times 10^{-5}\text{Pa}$  ( $4.0 \times 10^{-7}\text{Torr}$ ). First, it is transported to a first seed layer forming chamber to form a first seed layer 2 of Ni-25at.%Cr-15at.%Zr with a thickness of 20nm under the condition of Ar atmosphere about 0.8Pa (6mTorr) by the DC magnetron sputtering method. Subsequently, it is

transported to a second seed layer forming chamber to form a second seed layer 3 of Co-40at.%Cr-5at.%Zr with a thickness of 50nm under the condition of Ar atmosphere about 0.8Pa (6mTorr) by the DC magnetron sputtering method. Subsequently, it is transported to a heating chamber in the vacuum layer to heat the substrate to the substrate temperature 260°C by an infrared heater.

Subsequently, it is transported to an under layer forming chamber to form an alloy under layer 4 of Cr-10at.%Mo-7.5 at.%Ti with a thickness of 30nm under the condition of Ar atmosphere about 0.8Pa (6mTorr) by the DC magnetron sputtering method. Subsequently, it is transported to a magnetic recording layer forming chamber to form an alloy layer 5 (to form a magnetic layer) of Co-20at.%Cr-4at.%Ta-8at.%Pt with a thickness of 22nm under the condition of Ar atmosphere about 0.9Pa (7mTorr) by DC magnetron sputtering method. By using the substrate where the alloy under layer 4 of Cr-10at.%Mo-7.5 at.%Ti and the alloy layer 5 of Co-20at.%Cr-4at.%Ta-8at.%Pt are formed, the protective coating layer which is mentioned later and mainly composed of carbon according to the invention is formed.

As the substrate 1, in addition to the soda lime glass, used is a non-magnetic rigid substrate formed of chemical reinforced aluminosilicate, an Al-Mg alloy electroless-plated with Ni-P, silicon, ceramics made of borosilicate glass or the like, or ceramics subjected

to glass glazing or the like.

As the first and second seed layers are provided for avoiding electrochemical precipitation of alkali metal from the soda lime glass, they may have an arbitrary thickness, and one layer will do. Further, if not needed, it may be omitted. The under layer 4 is used as a under film for controlling the crystal orientation of a magnetic layer formed thereon. As the under layer, used is a thin film of a Cr-group alloy such as non-magnetic Cr-V, Cr-Ti, Cr-Mo, Cr-Si, Cr-Mo-Ti alloy forming an irregular solid solution which has good crystal consistency with the magnetic film and may be (100) orientated. When simultaneously 0.5 vol.% to 50 vol.% nitrogen is added to the gas for discharge used in sputtering to form the under layer, the crystal grains of the under layer are refined. As a result, the crystal grains of the continuously formed magnetic layer are also refined so that medium noise can be reduced.

As the magnetic layer 5, not only Co-Cr-Pt-Ta alloy, but a multi-alloy family material in which Co is taken as principal component, Pt is contained to increase the coercive force, and further Cr, Ta, SiO<sub>2</sub>, Nb and the like to reduce medium noise are added may be used. Especially, when Ta, Nb, V, and Ti are added, the melting point of a target is lowered, and composition separation of the magnetic film containing Cr is easy to progress. This is favorable.

In the Co-group alloy family material to which Pt, Ni or Mn is added, lowering of magnetic anisotropic energy is less than that in the case of other additive elements, so it is practical. To be concrete, in addition to Co-Cr-Pt, used are alloys such as Co-Cr-Pt-Ta, Co-Cr-Pt-SiO<sub>2</sub>, Co-Cr-Pt-Mn, Co-Cr-Nb-Pt, Co-Cr-V-Pt, Co-Cr-Ti-Pt, Co-Cr-Nb-Ta-Pt, Co-Pt-Ni-SiO<sub>2</sub> and the like.

Concerning the composition of a Co alloy layer occupying a ferromagnetic portion, it is considered that the solid solution limit of Cr is 5 to 10at.%, and the solid solution limit of Ta is about 2at.%, and a Co alloy magnetic layer is formed exceeding these solid solution limits, whereby the magnetic separation in the magnetic layer progresses to reduce medium noise. As a practical composition, for example, the followings are used:

Co-20at.%Cr-4at.%Ta-8at.%Pt alloy;  
Co-22at.%Cr-20at.%Pt alloy;  
Co-15at.%Cr-8at.%Pt-20mol.%SiO<sub>2</sub> alloy;  
Co-17at.%Cr-12at.%Pt-5at.% Mn alloy;  
Co-17at.%Cr-5at.%Nb-10at.% Pt alloy;  
Co-20at.%Cr-5at.%V-12at.%Pt alloy;  
Co-20at.%Cr-10at.%-15at.%Pt alloy;  
Co-15at.%Cr-5at.%Nb-5at.%Ta-20at.%Pt alloy.

The above substrate is transported without being taken out from the vacuum vessel to a protective coating layer forming chamber 21 shown in Fig. 2. The protective coating forming chamber 21 is formed by an

ion gun including a heat filament 22, an anode 23 and a grid 24 disposed in front of the heat filament. While the protective coating forming chamber 21 is evacuated by a turbo-molecular pump, from the rear of the anode, 5 15sccm (Standard Cubic centimeter per minutes) of Ar gas, 50sccm of ethylene ( $C_2H_4$ ) gas, further 20sccm of carbon dioxide ( $CO_2$ ) gas, 10sccm of nitrogen dioxide ( $NO_2$ ) gas and 10sccm of laughing gas ( $N_2O$ ) are introduced through a mass flow controller. At this 10 time, the pressure is about 0.5Pa(4mTorr) at the baratron gauge.

Subsequently, 30A is applied to the heat filament of the ion guns positioned on both sides of the substrate, DC +100V is applied to the anode to induce 15 plasma, and then -530V is applied to the grid to derive ions. Further, pulse bias with -100V and 3kHz is applied to the substrate. At this time, the anode current is 500mA, and the bias current of the substrate is 50mA. By this ion beam deposition method (IBD), a 20 DLC protective coating layer 6 mainly composed of carbon and hydrogen is formed 3nm thick on the Co-Cr-Ta-Pt alloy layer 5. The deposition rate of coating at this time is 1.0nm/s.

By the above method, plural discs are 25 manufactured, some of them are subjected to thin film analysis, and the other are provided with a lubricant layer 7 of fluorocarbon family. The thickness of the layer is 2.2nm measured by quantitative analysis using

Fourier-Transform InfraRed spectroscopic analyzer (FT-IR). After that, floating check is performed to make a sliding test in a single plate, or the disc is built in the magnetic disc apparatus to make a reliability test.

5           The protective coating of the disc manufactured by the above method is analyzed by the following methods to measure the proportion of functional groups of the protective coating surface. That is, ESCA (Electron Spectroscopy for Chemical Analysis) is used  
10 for identifying the covering rate of the functional groups of the protective coating surface. Direct identification of  $\text{-COOH}$ ,  $\text{-C=O}$ ,  $\text{-COH}$ ,  $\text{-CNH}_2$  which are surface functional groups, using ESCA is difficult in view of sensitivity and measurement accuracy. The  
15 above problems have been overcome by the tag modification method described in the following.

That is, the covering rate identification is performed by modification (tag modification) using molecules which have functional groups interacting with  
20 the protective coating surface functional groups quantitatively and irreversibly by molecular recognition, and contain fluorine atoms which have high sensitivity coefficient to ESCA .

To be concrete,

25           • To identify  $\text{-COOH}$  functional group, the protective coat surface is dipped in a benzene solution of pentafluorophenyl bromide for one hour to modify  $\text{-COOH}$  functional group with fluorine molecules.



• To identify  $-C=O$  functional group, the protective coating surface is dipped in an ethanol solution of pentafluorophenylhydrazine for one hour to modify  $-C=O$  functional group with fluorine molecules.

5       • To identify  $-COH$  functional group, the protective coating surface is dipped in an ethanol solution of perfluorooctyldimethylchlorosilane to modify  $-COH$  functional group with fluorine molecules.

10       • To identify  $-CNH_2$  functional group, the protective coating surface is dipped in a chloroform solution of pentafluorobenzoylchloride for one hour to modify  $-CNH_2$  functional group with fluorine molecules.

15       The respective protective coating surface tag-modified by one hour reaction at room temperature are dipped in the respective solvents to remove unreacted material from the protective coating surface.

20       In identifying the functional group covering rate of the protective coating surface, each tag-modified protective coating surface is obtained at an angle  $24^\circ$  of analysis of ESCA by Cls and Fls measurement intensity ratio, and as a result, the proportion of the functional groups  $-COOH$ ,  $-C=O$ ,  $-COH$ ,  $-CNH_2$  per 100 carbon atoms is about 30% on the average in total.

25       On the other hand, the disc provided with a lubricant is attached on an evaluating apparatus having a head load/unload mechanism to make a test. When load/unload test on ten discs are made 50000 times at a rotating speed of 15000 r.p.m, tests on all of ten

discs are ended without crash. Further, when the thickness of the lubricating layer of the tested disc is measured by FT-IR, it is confirmed that the thickness is hardly decreased, 2.1nm. As a result, it is proved that the magnetic recording medium of the invention has reinforced bonding force to the lubricant so that a decrease in lubricant due to spin-off is small, and even in the case where the thickness of the protective coating is very thin, 3nm, sliding resisting reliability is sufficient. The above evaluation result is described as sample No. 1 in Fig. 3.

<Comparative Example>

Sample No. 2 is manufactured by the substantially same method as that of the embodiment 1 except that 10sccm of carbon dioxide (CO<sub>2</sub>) gas and nitrogen oxide (NO<sub>2</sub>) gas and dinitrogen monoxide are not added at the time of forming the protective coating layer 6. The thickness of the protective coating layer 6 is 3nm which is the same as that of the embodiment 1, and similarly the thickness of the lubricating layer 7 is 2.2nm. The thus manufactured disc is evaluated by the same method as that of the embodiment 1.

As a result, in the tag modification analysis, the proportion of the surface functional group is 13%. When load/unload test is made on ten discs at the rotating speed of 15000 r.p.m, all of the discs cause crash during the time from 1000 times to 8000 times. When the thickness of the lubricating layer is measured

on ten discs by FT-IR, it is confirmed that the thickness is decreased to 0.7 to 1.2nm as compared with that before the test.

As a result, it is known that in the magnetic recording medium obtained by the manufacturing method of the comparative example, the bonding force between the protective coating layer and the lubricating layer is not enough so that the lubricating layer is scattered and decreased due to high speed rotation, and the frictional force between the magnetic recording medium and the magnetic head is increased to cause crash.

<Embodiment 2>

When 5,0000 times load/unload tests are executed on the disc described in the embodiment 1, in all of the magnetic recording medium taking the thickness of the magnetic film to be 15nm, 17nm and 21nm, the magnetic recording media and the magnetic head are not broken down, so favorable sliding resistance reliability is obtained.

By decreasing the thickness of the magnetic layer, the product  $B_r \times t$  of the thickness (t) of the magnetic layer and the residual magnetic flux density  $B_r$  is largely decreased. The in-plane coercive force  $H_c$  approximately ranges from 176kA/m to 256kA/m, the coercivity squareness  $S^*$  is from 0.74 to 0.65, about 0.7, and the remanence squareness is 0.78 to 0.7 (the remanence squareness  $S$  is the ratio of the residual

flux density to the saturated flux density). These magnetic characteristics are measured at 25 °C by a sample vibration type magnetometer.

5 The electromagnetic transducing characteristics of these magnetic recording medium are measured by using a magnetic head constructed so that the shield gap length  $G_s$  of the magnetoresistive reproducing element (MR element) is  $0.12\mu\text{m}$  and the gap length of the write element is  $0.2\mu\text{m}$ . The sense current of the  
10 MR element is set to 3mA, and the write current  $I$  is set to 41mA. The floating height of the head is varied by changing the rotating speed of the magnetic recording medium (magnetic disc medium) to measure the output half width PW 50 of a solitary reproduced wave by a  
15 digital oscilloscope (Tektronix TDS 544).

The thinner the magnetic film is, and the lower the floating height of the magnetic head is, the smaller the PW 50 is. In the case where the thickness of the magnetic film is 15nm and the floating height of  
20 the head is 25nm, a small value, 240nm is obtained. The output at the maximum track recording density of 360kFCI measured by the spectral analyzer is 1 to 2% of the output of a solitary reproduced wave at 10kFCI measured by the digital oscilloscope. The output at  
25 the maximum track recording density of 360kFCI measured by the spectral analyzer is integrated and obtained until it exceeds the output of waveform of the odd order by 100MHz.

Further, the ratio SLF/Nd of the integrated medium noise (Nd) in the case where 0-p output (SLF) of the solitary reproduced wave and a signal of 360kFCI are recorded is evaluated. The floating height of the head is taken as 25nm, and Nd is taken as the integrated value of noise of a band corresponding to from 0.5kFCI to 540kFCI. In all of media, a high SLF/Nd ratio above 24dB is obtained at the high recording density as much as 360kFCI.

Fig. 4 shows the constitution of the magnetic storage apparatus including the magnetic disc medium 61, a driving part 62 for driving the magnetic recording medium, a magnetic head 63 formed by a recording part and a reproducing part, a unit 64 for moving the magnetic head relatively to the magnetic recording medium, a signal input unit for inputting a signal to the magnetic head, a recording reproducing signal processing unit 65 for reproducing an output signal from the magnetic head, and a part 66 serving as a refuge place at the time of loading and unloading the magnetic head.

The reproducing part of the magnetic head is formed by a magnetoresistive head. Fig. 5 is a typical perspective view of the magnetic head used in measurement. The head is a composite head having both an electromagnetic induction type head for recording and a magnetoresistive head which are formed on a substrate 601. The recording head is formed by an

upper recording magnetic pole 603 and a combined lower recording magnetic pole and upper shield layer 604 which sandwich coils 602, and the gap length between the recording magnetic poles is  $0.3\mu\text{m}$ . For the coil, copper  $3\mu\text{m}$  thick is used. The reproducing head is formed by a magnetoresistive sensor 605 and electrode patterns 606 at both ends thereof, the magnetoresistive sensor is sandwiched by the combined lower recording magnetic pole and upper shield layer 604 and a lower shield layer 607 which are  $1\mu\text{m}$  thick, and the distance between the shield layers is  $0.20\mu\text{m}$ . In Fig. 6, the gap layer between the recording magnetic pole, and the gap layer 608 between the shield layer and the magnetoresistive sensor 608 are omitted.

Fig. 6 shows the structure of the section of the magnetoresistive sensor. The signal detection area 701 of the magnetic sensor is formed by a portion where a lateral bias layer 702, a separation layer 703 and a magnetoresistive ferromagnetic layer 704 are sequentially formed on a gap layer 700 of aluminum oxide. Ni-Fe alloy 20nm thick is used in the magnetoresistive ferromagnetic layer 704. Though Ni-Fe-Nb alloy 25nm thick is used in the lateral bias layer 702, any ferromagnetic alloy such as Ni-Fe-Rh and the like may be used if the electric resistance is comparatively high and soft magnetic characteristic is favorable.

The lateral bias layer 702 is magnetized by a

magnetic field formed by a sense current flowing through the magnetoresistive ferromagnetic layer 704 in the film in-plane direction (lateral direction) vertical to the current, and lateral bias magnetic field is applied to the magnetoresistive ferromagnetic layer 704. Thus, selected is a magnetic sensor showing the linear reproduction output to the leakage magnetic field from the medium 61. In the separation layer 703 for preventing effective shunt current of sense current from the magnetoresistive ferromagnetic layer 704, Ta having comparatively high electric resistance is used, and the film thickness is taken as 5nm.

Both ends of the signal detection area are provided with a taper part 705 worked to be tapered. The taper part 705 is formed by a permanent magnet layer 706 for making the magnetoresistive ferromagnetic layer 704 into single magnetic domain, and a pair of electrodes 606 formed thereon for taking a signal. It is necessary that the permanent magnet layer 706 has large coercive force and the magnetizing direction is not easily changed, and an alloy such as Co-Cr, Co-Cr-Pt or the like is used.

The magnetic storage apparatus shown in Fig. 4 is formed by combining the magnetic recording medium described in the embodiment 1 with the head shown in Fig. 5. As a result, in the floating system in which the magnetic floating height  $h_m$  is about 48 to 60nm, when the product  $Br \times t$  of the thickness ( $t$ ) of the

5 magnetic layer and the residual flux density  $B_r$  measured by applying a magnetic field in the relative running direction of the magnetic head to the magnetic recording medium in recording exceeds 9.6mA (120 gauss micron), satisfactory writing cannot be performed, the overwrite characteristic is deteriorated, and the output especially in the high track recording density area is also lowered.

10 On the other hand, when  $B_r \times t$  is smaller than 32mA (40 gauss micron), in some case, it is found that being left at 70°C for four days, the reproduction output is decreased in some composition or thickness of the recording layer of the medium. Accordingly, the magnetic storage apparatus is constructed so that the  
15 product  $B_r \times t$  of the thickness ( $t$ ) of the magnetic layer and the residual magnetic flux density  $B_r$  measured by applying a magnetic field in the relative running direction of the magnetic head to the magnetic recording medium in recording mentioned in the magnetic  
20 recording medium described in the embodiment 1 ranges from 3.2mA (40 gauss micron) to 9.6mA (120 gauss micron) both inclusive.

25 In the case where the magnetoresistive sensor part of the magnetoresistive head uses a head formed between two shield layers which are spaced from each other at a distance of 0.2 $\mu$ m and made of soft magnetic substance, when the maximum track recording density exceeds 250kFCI, sufficient reproduction output cannot



be obtained. When the distance between two shield layers made of soft magnetic substance is below  $0.12\mu\text{m}$ , the element cannot be formed easily because of difficulty in process machining. Accordingly, the magnetic storage device is formed by using a head formed between two shield layers which are spaced from each other at a distance ranging from  $0.12\mu\text{m}$  to  $0.2\mu\text{m}$  both inclusive and made of soft magnetic substance. By the thus constructed magnetic storage apparatus, the recording density equal to or higher than 50 giga bit per  $1\text{ in}^2$  can be realized.

<Embodiment 3>

A magnetic storage apparatus is formed by the same constitution as that of Fig. 4 except that instead of the magnetoresistive head used in the embodiment 2, the magnetoresistive head 63 described in the embodiment 2 uses a magnetic head formed by a magnetoresistive sensor including plural conductive magnetic layers which cause a large resistance change due to a relative change in mutual magnetizing directions by an external magnetic field and a conductive non-magnetic layer disposed between the conductive magnetic layers.

Fig. 7 shows the sectional view of the used sensor. The sensor has a structure in which a Ta buffer layer 801 5nm thick, a first magnetic layer 802 with a thickness of 7nm, an intermediate layer 803 made of copper 1.5nm thick, a second magnetic layer 804 3nm

thick, and a Fe-50at.%Mn antiferromagnetic alloy layer 805 10nm thick are sequentially formed on a gap layer 608. In the first magnetic layer 802, Ni-20at.%Fe alloy is used, and in the second magnetic layer 804, cobalt is used.

By exchange magnetic field from the antiferromagnetic layer 805, the magnetization of the second magnetic layer 804 is fixed in one direction. On the contrary, the direction of the first magnetic layer 802 which is in contact with the second magnetic layer 804 by intercalating the non-magnetic layer 803 is varied by the leakage magnetic field from the magnetic recording medium 61 so that the resistance change is caused.

Such resistance change caused by a change in the relative direction of magnetization of two magnetic layers is called spin valve effect. In the present embodiment, a spin valve head utilizing the effect for the reproducing head is used. The taper part 705 has the same constitution as that of the magnetic sensor of the embodiment 2.

The  $B_r \times t$  of the magnetic recording medium used in measurement is taken as 3, 3.2, 4, 6, 8, 10, 12, and 14mA. In the case where  $B_r \times t$  is taken as 3mA (37.5 gauss micron), lowering of a reproducing signal caused with the passage of time is extreme, and it is difficult to obtain practically favorable coercive force. When  $B_r \times t$  exceeds 12mA (150 gauss micron),

though the output of 2F is large, the tendency of lowering the output resolution becomes remarkable so that it is not favorable.

When such a spin valve reproducing head is used,  
5 as described in the embodiment 2, a signal recorded at the maximum track recording density exceeding 360kFCI is stably reproduced to obtain signal output.

The head shown in here is the same as the head used in the embodiment 2, and the magnetoresistive head  
10 is formed on the magnetic head slider constructed so that the area of the floating surface rail is equal to or smaller than  $1.4\text{mm}^2$  and the mass is equal to or less than 2mg. Setting the area of the floating surface rail equal to or smaller than  $1.4\text{mm}^2$  reduces the  
15 probability of colliding with the projection, and simultaneously setting the mass equal to or less than 2mg can improve shock resistance reliability. Thus, high recording density and high shock resistance can be reconciled, and the average failure time interval  
20 (MTBF) equal to or longer than 30,000 hours at the recording density equal to or higher than 50 giga bit per  $1\text{ in}^2$  can be realized.

According to the invention, the bonding performance between the protective coating and the  
25 lubricating film can be reinforced. Furthermore, a mass-stored and high reliability magnetic disc apparatus can be provided by combining the magnetic recording medium with the magnetic head.